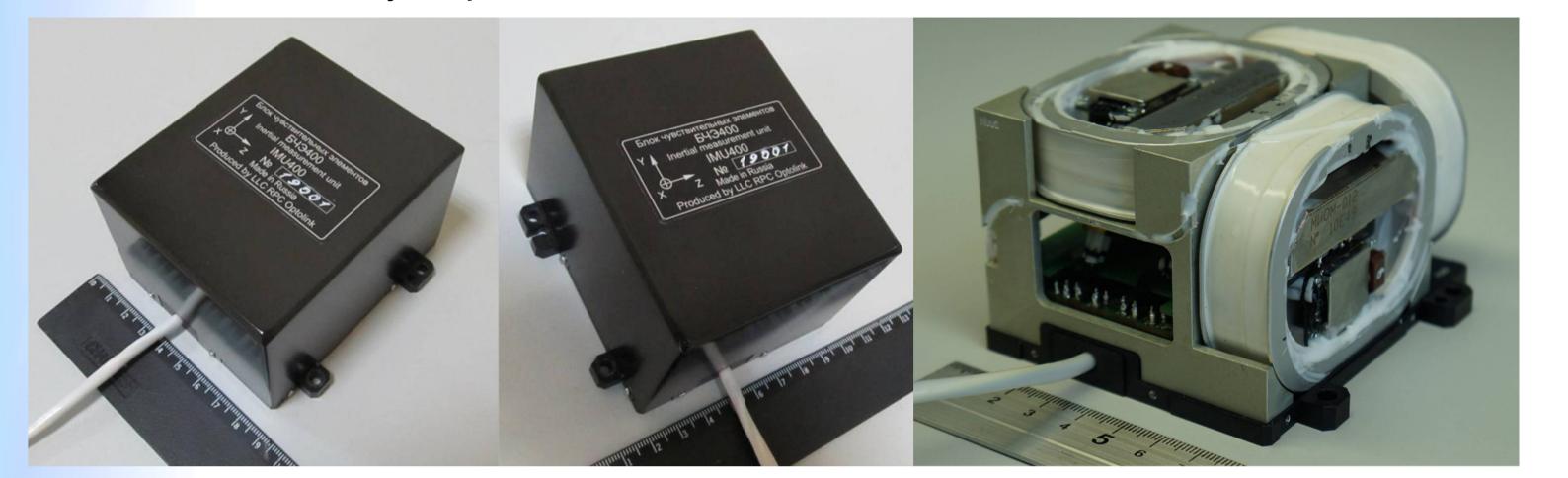
## **Ultra-compact navigation-grade Inertial Measurement Unit IMU400**

Yu.N. Korkishko, V.A. Fedorov, V.E. Prilutskiy, V.G. Ponomarev, S.V. Prilutskiy, D.V. Obuhovich, I.V. Fedorov, A.I. Zuev, V.K. Varnakov, S.M. Kostritskii, I.V. Morev

## **CD OPTOLINK RPC LLC, Moscow, Russia** Fiber Optical Solution, Riga, Latvia

At present time interferometric fiber-optic gyroscopes (IFOGs) are widely used in inertial navigation systems (INS), and in wide range of applications have replaced its well-established main competitor ring laser gyroscopes (RLG). In high precision closed-loop configuration of IFOG the feedback mechanism keeps the zero signal level by compensating the Sagnac phase shift with additional phase counter-shift. The value of the phase counter-shift allows one to obtain information about the angular rate of the device rotation [1-4]. Due to its inherent low noise and its scalability, FOG technology is one of the very few technologies able to cope with the applications requiring the highest performance combined with cost and SWaP.

Recently, in order to cover the mass-market applications spectrum requiring lowcost and compact inertial sensor yet as much precise as it can be, Optolink has launched new product: ultra-compact navigation-grade inertial measurement unit IMU400. External and internal view (gyro coils) of IMU400 is shown in Figure 1. The aim of the current work was the production of pilot IMU400 devices batch and the estimation of the performance of IMU with direct approach and also with strapdown inertial navigation systems (SINS) simulation methods, which by sense is indirect way of performance observation.



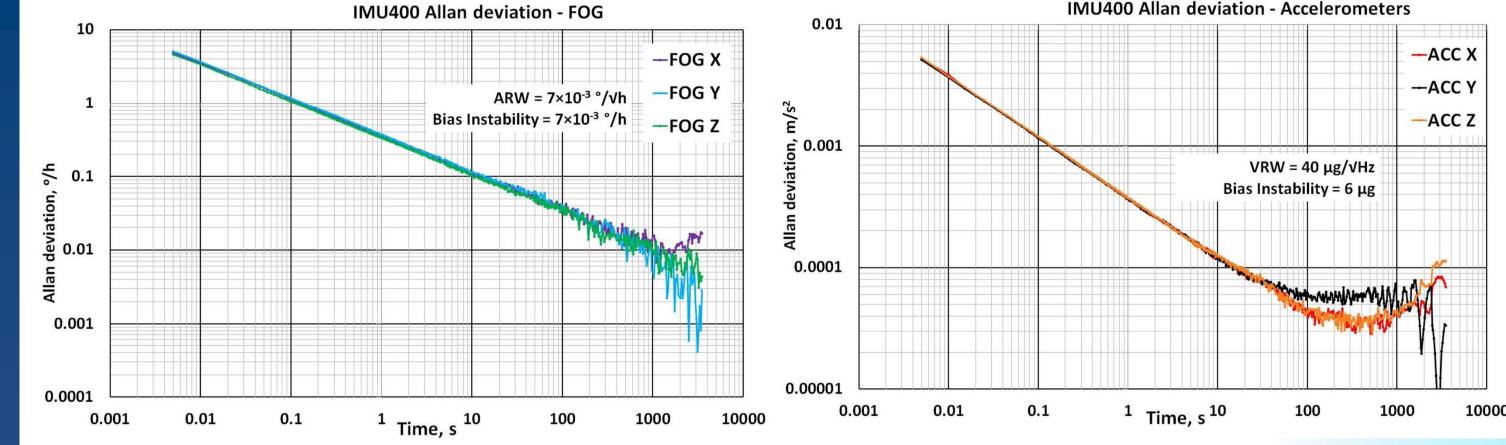


Figure 3. IMU400 FOG and ACC channels Allan variance plots

Figure 1. IMU400 external and internal view (gyro coils). **IMU400** SWaP properties are:  $80 \times 95 \times 62$  mm, 0.7 kg, 0.5 l,  $\leq 7$  W. FOGs are fed with single light source, coils are designed in the shape of rectangle with rounded corners. To cut down the size and cost, regularly used quartz pendulous accelerometers were substituted by MEMS, the IMU has 3 triads (physical) of MEMS accelerometers, with 6 low-noise (composing 2 effective triads) and 3 high-noise acceleration channels which are neglected.

IMU400 specification is shown in Table 1. Its Allan variance amo Optolink's FOGs is shown in Fig According to regular Allan Varia results (fFg.3), IMU400 per values are: - Gyroscope axes ARW 0.007 °  $/\sqrt{hour}$ , bias 0.01 ° /hour, run-to-run 0.015 100 factor scale error Accelerometers - VRW 40  $\mu g/\sqrt{}$ instability 6 µg, run-to-run 20 µ factor error 150 ppm. In Fig. 4 IMU400 bias stability (c in temperature range -40° C with constant temperature cha (ramp) +20° C/hour (20+) 20° C/hour (20-) are shown. values are shifted. In temperature range IMU400 also shows stable behavior ( Figure 4), with gyro and ACC (100s-averaging RMS,  $<0.1^{\circ}$  /hour and  $<100\mu g$ .

**Bias Instability** 

1

0.1

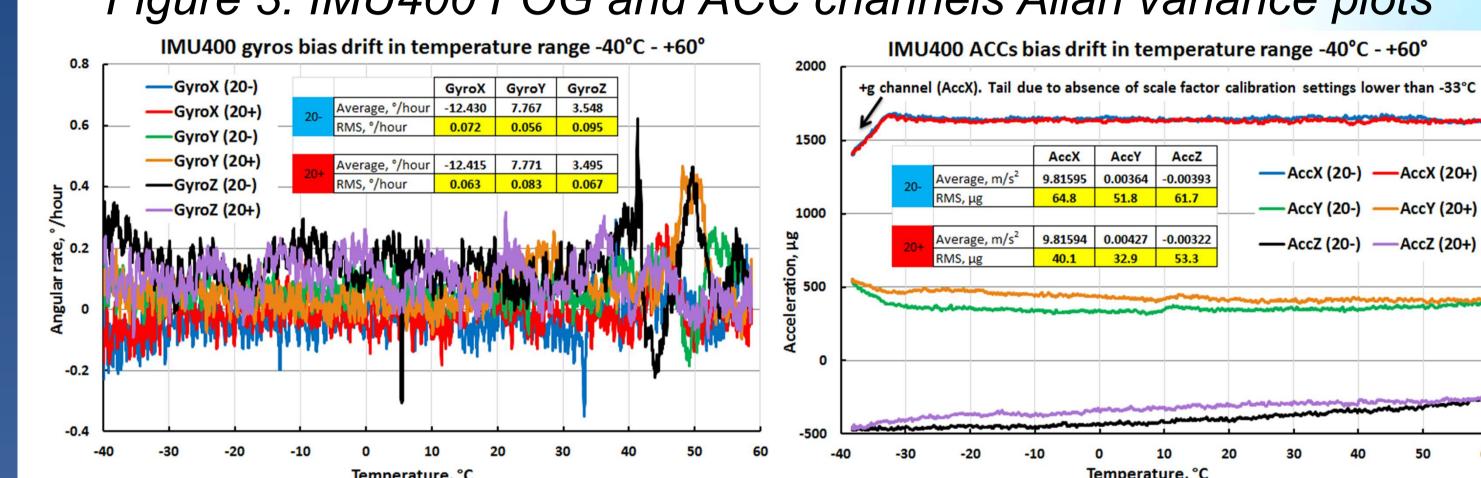
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5 SHOWN III		
e among other	Performance	IMU400
in Fig. 2.	Gyro	
Variance plot	Angular rate range, °/s	±550
performance	Bias drift at constant temperature (1σ, 100s-averaging), °/h	0.1
axes (FOG) - bias instability	Bias drift (1σ, 100s-averaging) in operational temperature range, °/h	0.7 (*0.3)
0.015 ° /hour,	Angle random walk, °/ √h	0.01
	Scale factor error, ppm	500 (*200)
100 <sub>,</sub> ppm;	Bandwidth, Hz	> 1000
µg/√Hz, bias	Accelerometers	
20 µg, scale	Range, g	±10
	Bias drift at constant temperature, mg	1
ility (drift) plots	Bias drift in operational temperature range, mg	1.0 (*0.4)
$0^{\circ} C - +60^{\circ}$	Scale factor error, ppm	500 (*300)
e change rate	Noise power density, mg/ VHz	0.08
<b>U</b>	Bandwidth, Hz	> 300
0+) and -	Physical Characteristics	
own. Absolute	Misalignment, °	0.08 (*0.015)
	Output sample rate, Hz	up to 2000
400 pilot units	Power supply, V / Consumption, W	5 / 7
-	Digital output interface	RS-422
vior (shown in	Operational temperature range, °C	<b>-</b> 40 ~ +60
ACC bias drift 1σ) of	Dimensions, mm	$80 \times 95 \times 62$
	Weight, kg	0.7
Optolink FO	Gs Allan Variance	
	$\frac{IMU400}{ARW = 6 \times 10^{-3} ^{\circ}/Vh}$ $\frac{IMU500}{Sias Instability = 6 \times 10^{-3} ^{\circ}/h}$ $\frac{IMU500, TRS500}{ARW = 4.4 \times 10^{-3} ^{\circ}/Vh}$ $\frac{IMU500, TRS500}{ARW = 1.4 \times 10^{-3} ^{\circ}/Vh}$ $\frac{SRS501}{ARW = 2.1 \times 10^{-3} ^{\circ}/Vh}$	0 0, TRS500 L (Space) 00
	Bias Instability = $1 \times 10^{-3}$ °/h	BIS (Space Grade)

OBIS (Space Grade

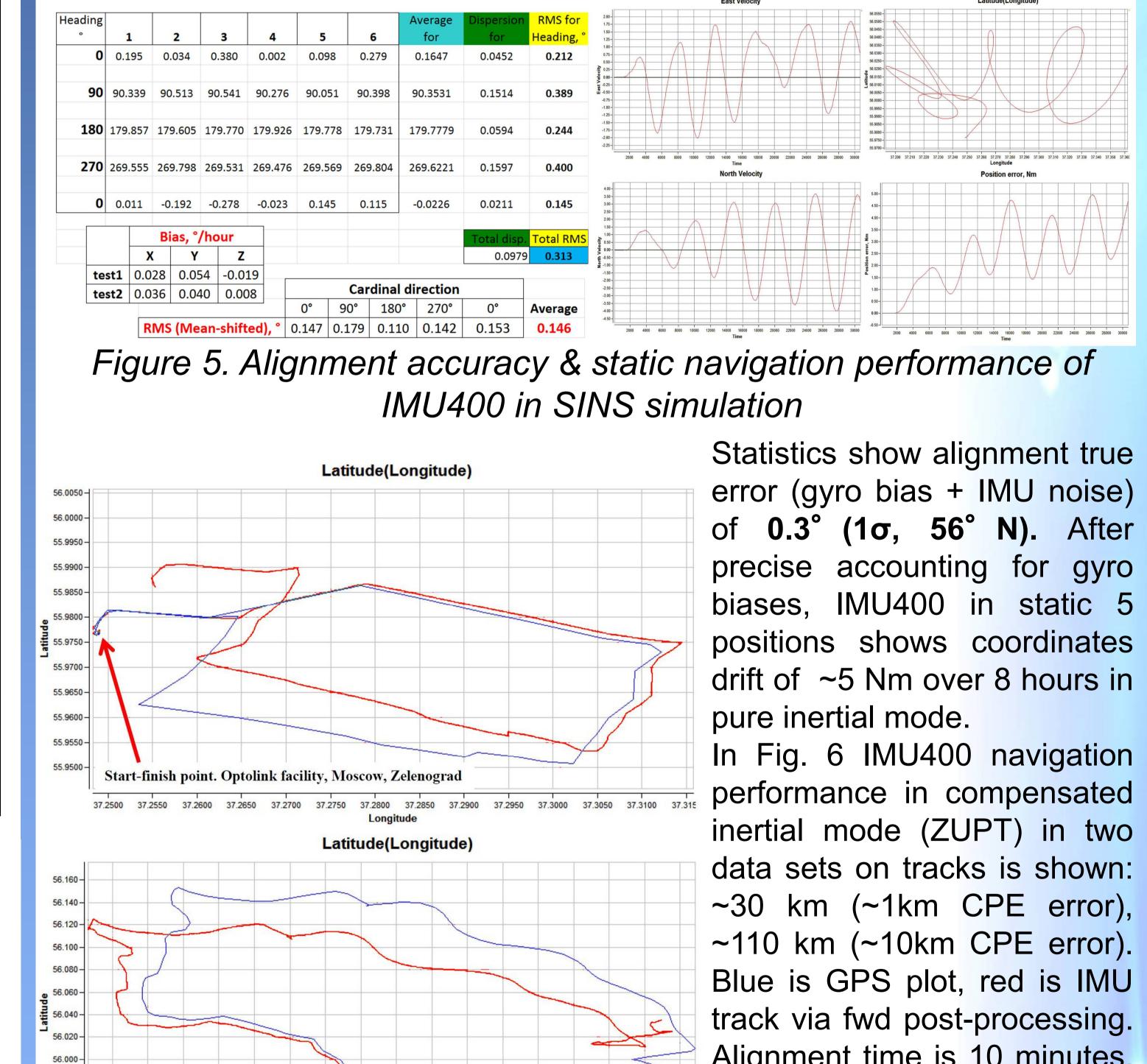
ARW =  $2.4 \times 10^{-3}$ °/vh

Bias Instability = 1×10<sup>-3</sup> °/h

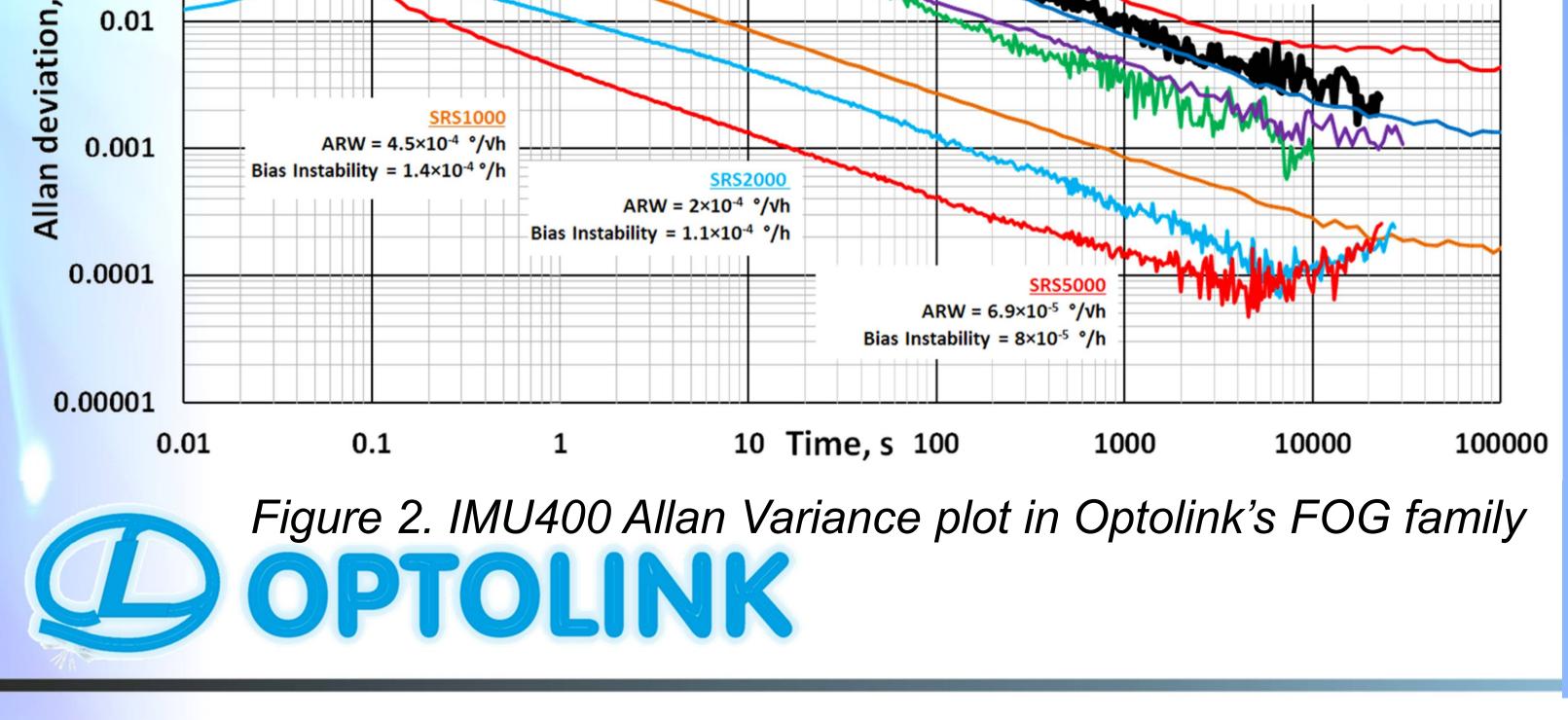


## Figure 4. IMU400 Gyroscopes & Accelerometers bias stability plots

At Optolink [5], for SINS certain test procedures are carried out in order to qualify their accuracy level. One of the main and peculiar SINS parameters is the obtained heading accuracy during straightforward alignment in gyrocompassing mode. The performance of IMU400 units was then investigated using these indirect way of measurements (Fig. 5,6).



In Fig. 6 IMU400 navigation performance in compensated inertial mode (ZUPT) in two data sets on tracks is shown: ~30 km (~1km CPE error), ~110 km (~10km CPE error). Blue is GPS plot, red is IMU track via fwd post-processing. Alignment time is 10 minutes. 55.980-Shown in Fig. 5,6 values are 55.960several orders better than any 55.940-Start-finish point. Optolink facility, Moscow, Zelenograd 55.920-MEMS or open-loop FOG for the same task (not even Figure 6. IMU400 navigation performance measured in pure inertial (2 tracks: 1 – 30 km, 2 – 110 km length) mode). The observed performance values allow to assess IMU400 type of devices as navigation or near-navigation grade IMU with unique combination of performance / cost / SWaP characteristics. Edition. H.C. Lefevre, The Fiber-Optic Second [1] Gyroscope, Boston, Artech House, 2014 W.K. Burns, Ed., Fiber [2] Rotation Sensing, Optical Boston, Academic Press, 1994. [3] E. Udd and M. Digonnet, Eds., Design and Development of Fiber Optic Gyroscopes, Bellingham, Washington, SPIE Press, 2019. [4] H.C. Lefevre "The fiber-optic gyroscope: Achievement and perspective", Gyroscopy and Navigation, 2012, Vol.3, pp.223-226. [5] Yu.N.Korkishko et al., "Strapdown Inertial Navigation Systems Based on Fiber Optic Gyroscopes", Gyroscopy and Navigation, 2014, Vol. 4, No. 4, pp. 195–204.



## From optical components to navigation systems

LLC RPC «Optolink», Sosnovaya alley, d. 6A, building 5, module 3-1, Zelenograd, Moscow, 124489, Russian Federation Telephone: +7(495) 663-17-60; Fax: +7(495) 663-17-61; Web-site: www.optolink.ru; E-mail: opto@optolink.ru